

# RMIT SKYHOOK ENGINEERS

Undergraduate Team



## EXECUTIVE SUMMARY

36TH ANNUAL STUDENT DESIGN  
COMPETITION

EXTREME ALTITUDE MOUNTAIN RESCUE VEHICLE



**AIRBUS**



# 2019 Skyhook Engineers Team

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## Consent and Request

The RMIT Skyhook Engineers consent to publication of the Executive Summary on the Vertical Flight Society's website. Additionally, the RMIT Skyhook Engineers wish to receive feedback on their design.

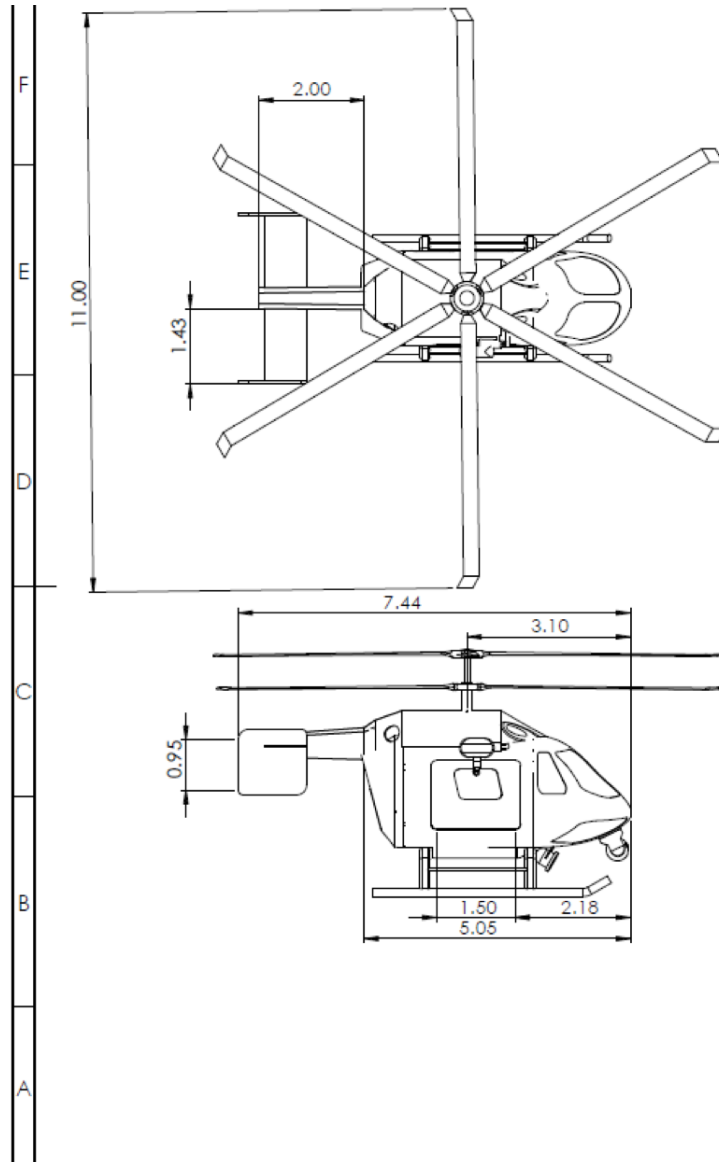


## DROP BEAR General Characteristics

<b>Maximum take-off weight</b>	<i>2,741.48 kg</i>	<i>6043.93 lbs</i>
<b>Empty Weight</b>	<i>1,956.48 kg</i>	<i>4313.3 lbs</i>
<b>Useful Load fraction</b>	<i>785 kg</i>	<i>1730.63 lbs</i>
<b>Maximum cruise speed at sea level</b>	<i>273.6 km/h</i>	<i>147.7 knots</i>
<b>Hover ceiling</b>	<i>9,327 m</i>	<i>30,601 ft</i>
<b>Maximum range at sea level</b>	<i>309.3 km</i>	<i>167 n miles</i>
<b>Maximum Endurance at sea level</b>	<i>2.53 hours</i>	<i>2.53 hours</i>



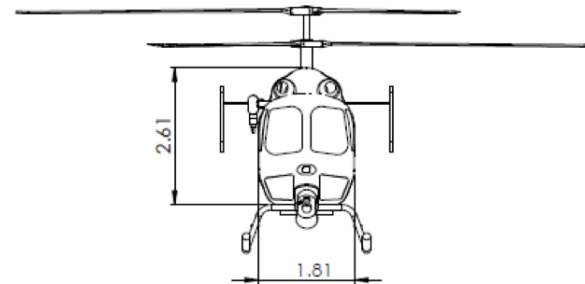
# DROP BEAR Dimensions



SCALE 1:80  
 MTOW 2,741.5 KG  
 Empty weight 1,956.48 KG

Hover ceiling 9,327 M  
 Maximum range at sea level 309.3 KM  
 Maximum endurance at sea level 2.53 Hours

ALL DIMENSIONS ARE IN METRES



UNLESS OTHERWISE SPECIFIED: DIMENSIONS ARE IN MILLIMETERS SURFACE FINISH: TOLERANCES: LINEAR: ANGULAR:			FINISH:	DEBURR AND BREAK SHARP EDGES	DO NOT SCALE DRAWING	REVISION
NAME	SIGNATURE	DATE	TITLE: RMIT SKYHOOK ENGINEERS - DROP BEAR SEARCH AND RESCUE HELICOPTER			
DRAWN: RMIT UNDERGRADUATE TEAM						
CHKD:						
APPVD:						
MFG:						
QA:			MATERIAL:	DWG NO.:	FINAL	A3
			WEIGHT: 2741.5 KG	SCALE: 1:80	SHEET 1 OF 1	

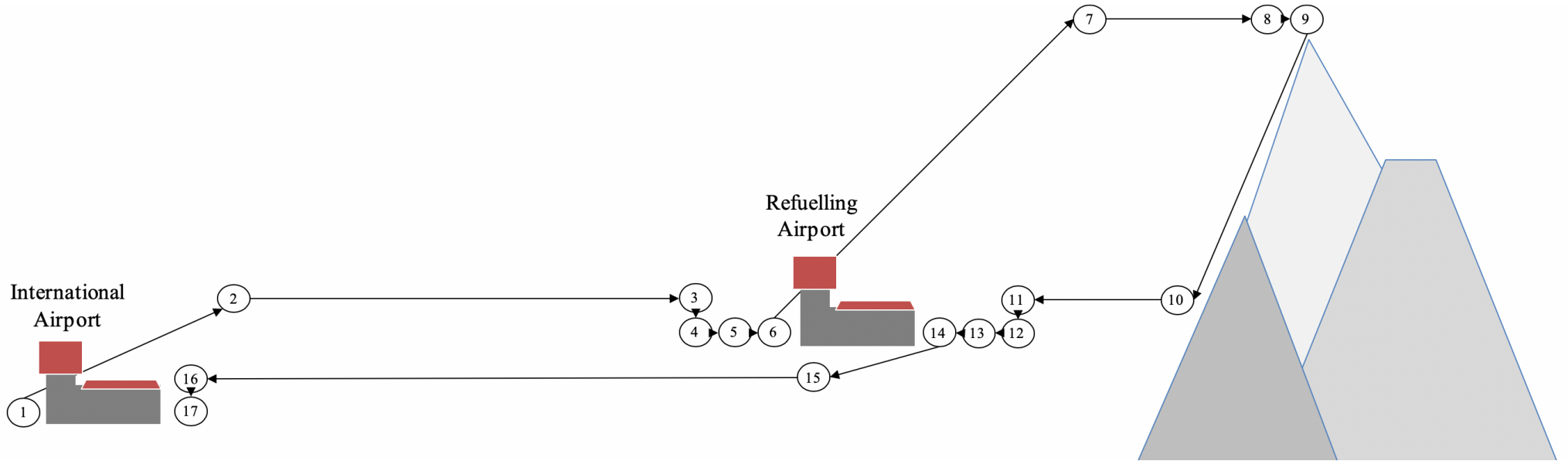


# Top-down mission requirements

- P The rotorcraft must complete the prescribed mission profile within 3 hours.**
- P The rotorcraft must be capable of extracting injured passengers in the worst-case scenario.**  
**Worst-case scenario is assumed to be unconsciousness.**
- P The rotorcraft must include a hoist system rated for 300 kg (662 lbs) with a minimum lifting load of 272.16 kg (600 lbs).**
- P The rotorcraft must include systems capable of surveying the ground and locating the injured passengers.**
- P The rotorcraft must be capable of maintaining heading in winds up to 74 km/h (40 knots) from any azimuth.**
- P The rotorcraft shall adhere to all FAA regulations and be certified for day and night IFR flight.**
- P All crew members must be capable of communicating with each other for the entirety of the mission.**



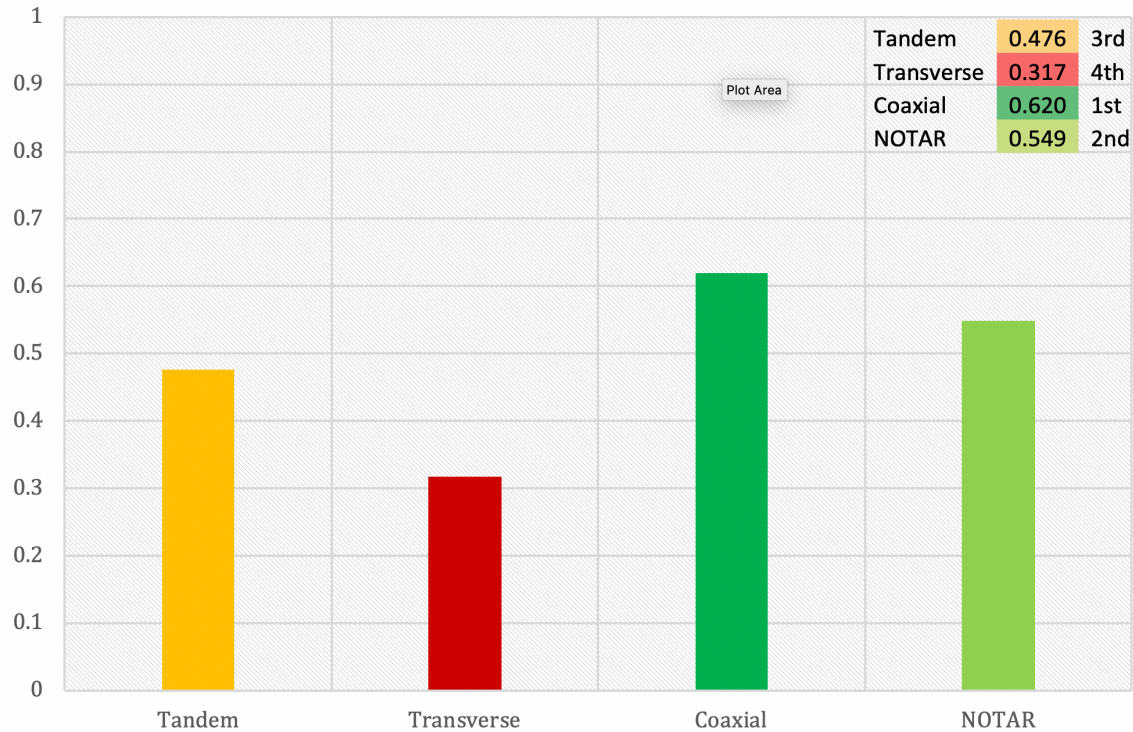
# Mission Profile



	START																	END	
		2 min hover	Climb	Cruise	2 min hover	20 mins	2 min hover	Climb	Cruise	30 min hover	Descent	Cruise	2 min hover	20 mins	2 min hover	Descent	Cruise	2 min hover	
Phase Number	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
Altitude	1402	1402	1402-3780	3780	3780	3780	3780	3780-8870	8870	8870	8870-3780	3780	3780	3780	3780	3780-1402	1402	1402	1402
Time [min]	0	2	2.62	35.6	2	20	2	5.75	4.69	30	3.03	6.9	2	20	2	2.25	35.41	2	178.2533968
$\Delta x$ [m]	0	0	4718.25	130281.75	0	0	0	14483.74	13516.26	0	2728.73	25271.27	0	0	0	5392.29	129607.71	0	0
$\Delta y$ [m]	0	~	2378	0	~	0	~	5090	0	~	5090	0	~	0	~	2378	0	~	0
Vx [m/s]	0	0	30	61	0	0	0	42	48	0	15	61	0	0	0	40	61	0	0
Vy [m/s]	0	0	15.12	0	0	0	0	14.76	0	0	-27.98	0	0	0	0	-17.64	0	0	0
Angle of attack [degrees]	0	90	26.75	0	90	0	90	19.36	0	0	61.8	0	90	0	90	23.8	0	90	0
Empty Weight	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37	1939.37
Available Turboshift [kW]	1343	1134	840.5	840.5	840.5	840.5	840.5	415.3	415.3	415.3	415.3	840.5	840.5	840.5	840.5	840.5	1134	1134	1134
Available Electric Engine [kW]	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494	494
Required Turboshift [kW]	0	673.3	840.5	812.8	720.5	0	720.5	415.3	415.3	415.3	423.785	812.8	720.5	0	720.5	504.7	971.4	673.3	0
Required Electric Engine [kW]	0	0	0	0	0	0	0	494	108.2	476.8	328.815	0	0	0	0	0	0	0	0
Fuel Weight [kg]	210	203.72	193.44	58.42	51.7	210	203.28	192.14	183.04	124.9	118.9	92.71	85.99	210	203.28	197.99	37.46	31.18	31.18
Payload Weight [kg]	405	405	405	405	405	405	405	405	405	575	575	575	575	575	575	575	575	575	150
Current Weight	2554.37	2548.09	2537.81	2402.79	2396.07	2554.37	2547.65	2536.51	2527.41	2639.27	2633.27	2607.08	2600.36	2724.37	2717.65	2712.36	2551.83	2545.55	2545.55

# Rotor Configuration Trade-off Analysis

Results of rotor configuration evaluation



**P** The highest scoring configuration is the Coaxial with a leading score of 0.62 compared to second place NOTAR at 0.55 and far succeeding Tandem with 0.48 and finally Transverse configuration with 0.32 points.

**P** Although there are mechanical complexities with the coaxial configuration it will be optimal and will require the use of the Prouty rotorcraft design method but modified for coaxial aircraft.

## Weighting criteria

Weighting value [%]

<b>Weight</b>	8	Hover ceiling	17.5
<b>Useful load</b>	5	Hovering stability	17.5
<b>Range</b>	7.5	Vibration	15
<b>Endurance</b>	6.25	Year of production	6.25
<b>Cruise Speed @ sea level</b>	5	Number of aircraft manufactured	4
<b>Cruise Speed @ altitude</b>	0.5	Cost	7.5



# Rotor Configuration

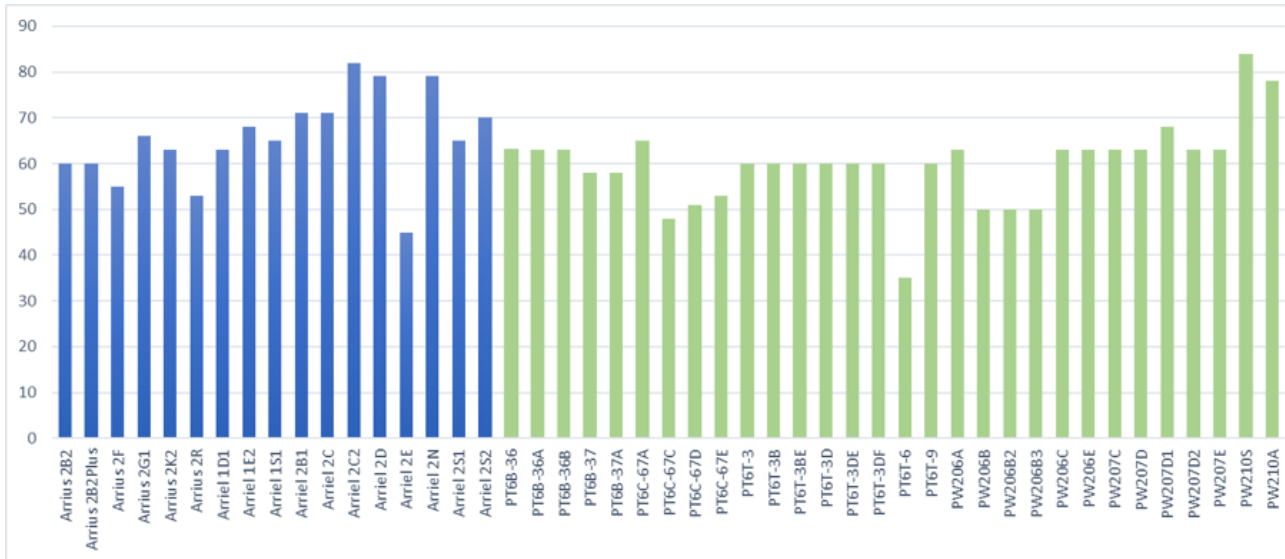
## Coaxial Rotor Configuration

**P** The Coaxial configuration has the contra rotating concentric two rotors on the same shaft and hence a zero-net torque for the system. Suitable for smaller cabins, proven design, improved hover stability, reduced roll tendencies. Disadvantages include mechanical complexities, high downwash velocities, poor forward cruise velocity, increased weight due to gearing, increased manufacturing and maintenance costs



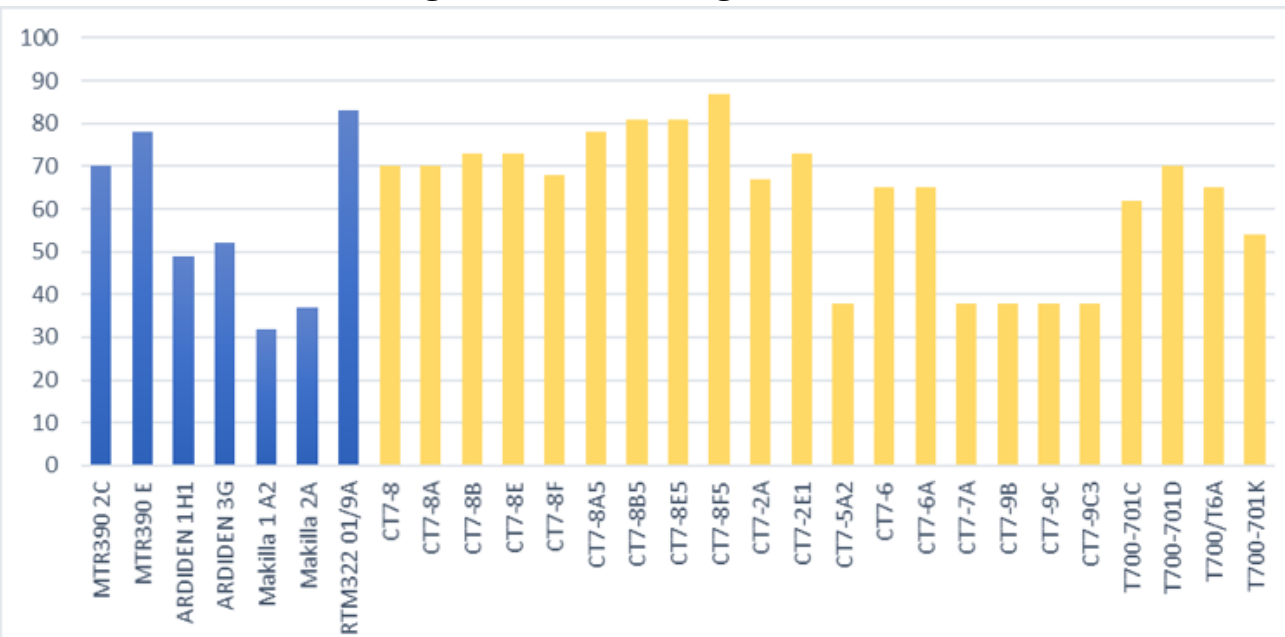
# Turboshaft Engine Trade-off Analysis

## Small turboshaft engine evaluation



The highest scoring small turboshafts are the PW210S, the Arriel 2C2, and the Arriel 2D and Arriel 2N. Of these engines, the Arriel 2N had the highest maximum continuous power and could meet our hover requirements when implemented in the hybrid propulsion package.

## Large turboshaft engine evaluation

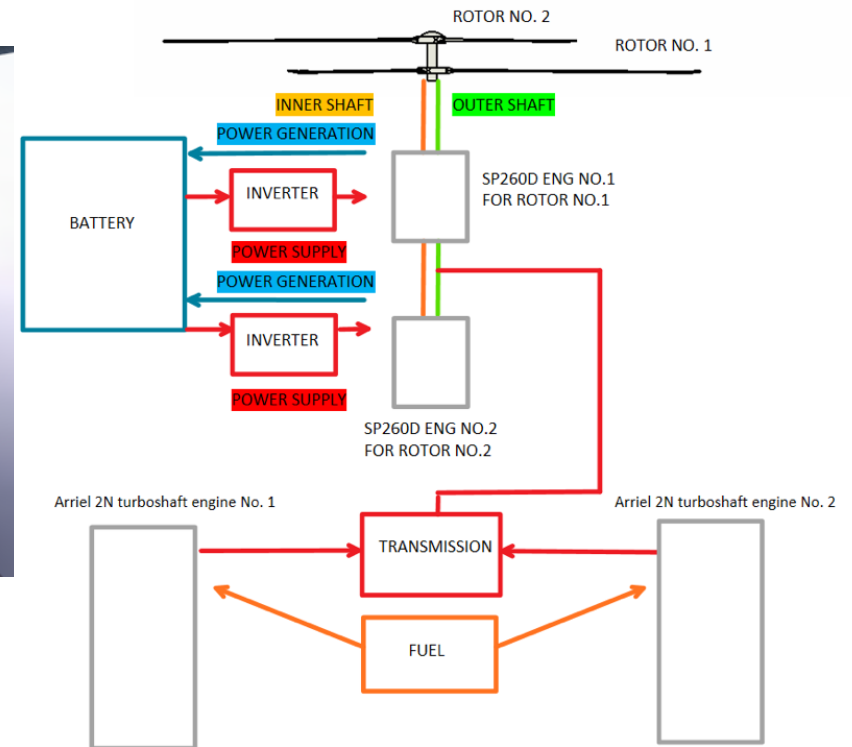
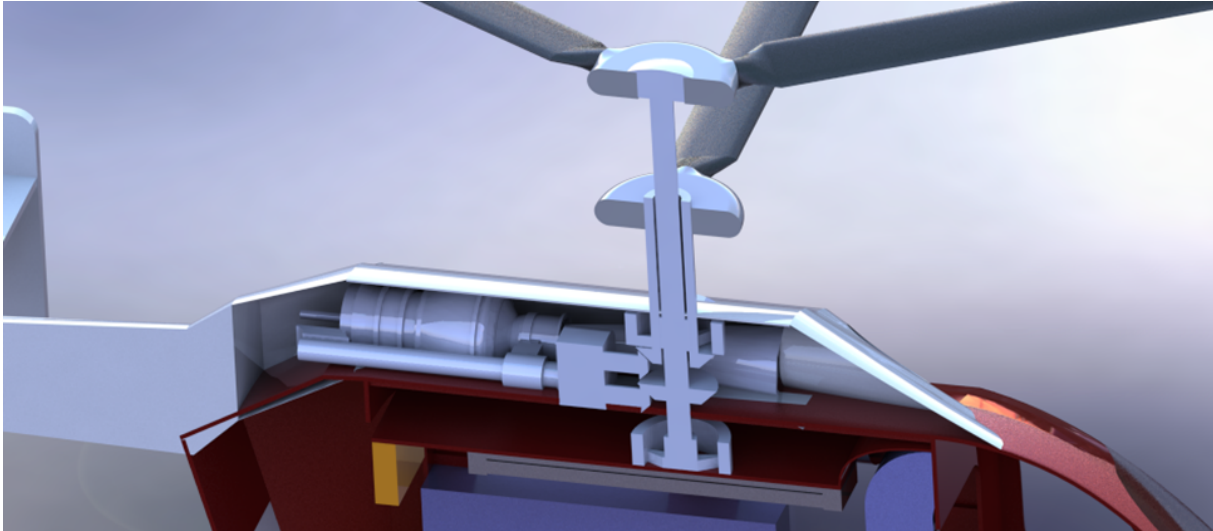


The highest scoring large engines are the CT7-8F5 and the RTM 322 01/9A. Both engines were tested in the turboshaft propulsion package, but neither could meet the hover requirements while maintaining a reasonable MTOW.



# Propulsion Configurations

## Hybrid Propulsion Package



For electric engine selection, the SP260D is selected since it was the only suitable electric engine currently available on the market for its specific attributes. Although not in service yet, legacy models have already been implemented in small fixed-wing aircraft such as the LE300, and the engine has a current TRL of 8.

### Electric Powerplant Specifications

2 Siemens SP260D Electric Engines		Manganese-Titanium (Lithium) Battery	
Engine Weight	100 kg	Battery Weight	150 kg
Power Output (ideal)	520 kW	Specific Energy	140 Wh/kg
Motor Efficiency	95%	Battery Energy	75.6 MJ
Power Output (real)	494 kW	Battery Volume	0.11 m <sup>3</sup>
Maximum RPM	2500	Minimum Temperature	-20°C



# Performance

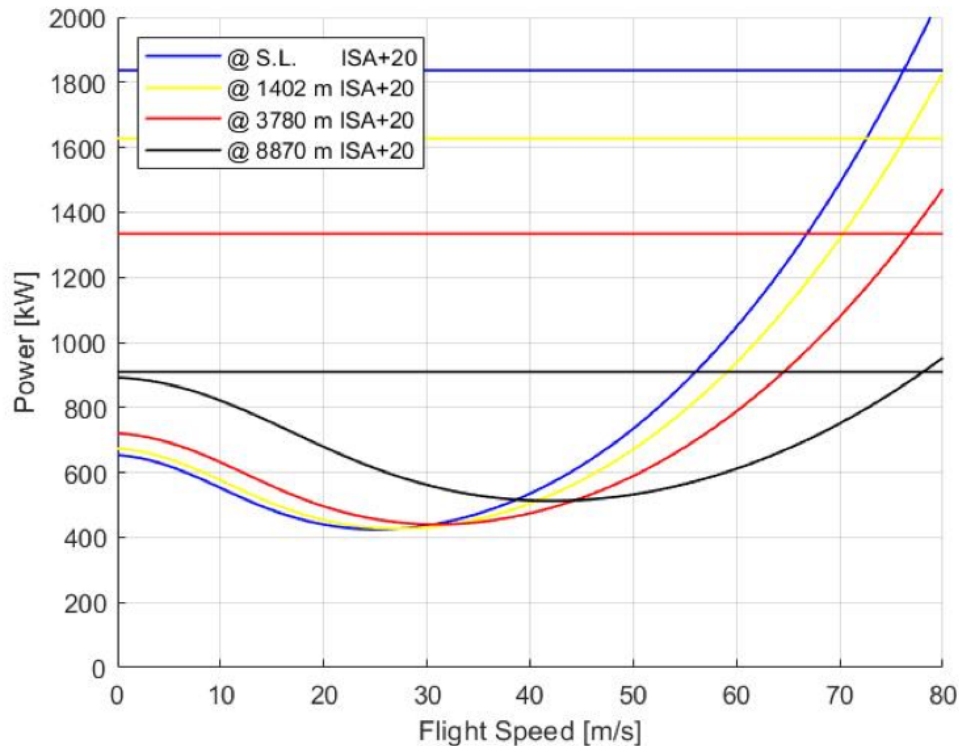
## Power Available

**P** The power available is a mixture of turboshaft and electrical availability.

### Power available for altitude

Altitude	Turboshaft Power	Electric Power	Power Available
Sea level	1,342.6 kW	494 kW	1,836.6 kW
1,402 m (4,600 ft)	1,133.9 kW	494 kW	1,627.9 kW
3,780 m (12,400 ft)	840.5 kW	494 kW	1,334.5 kW
8,870 m (29,100 ft)	415.3 kW	494 kW	909.3 kW

### Power required for forward flight



### Power required for hover

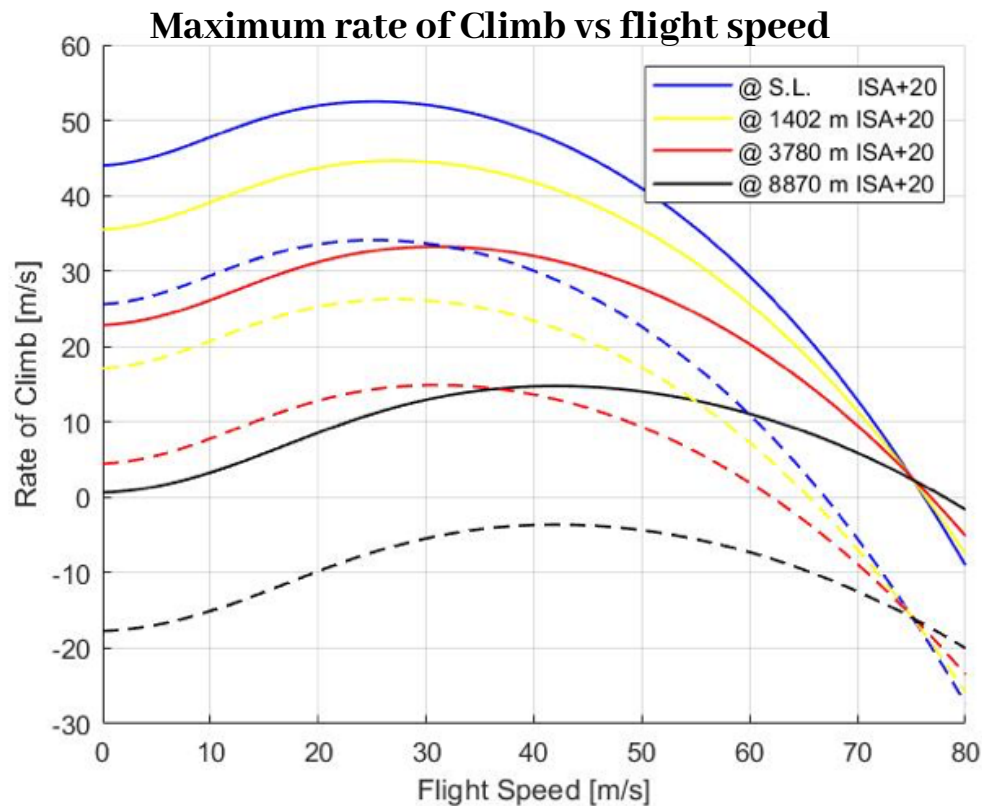
Altitude	Power required for hover
Sea level	653.5 kW
1,402 m (4,600 ft)	673.3 kW
3,780 m (12,400 ft)	720.5 kW
8,870 m (29,100 ft)	892.1 kW



# Performance

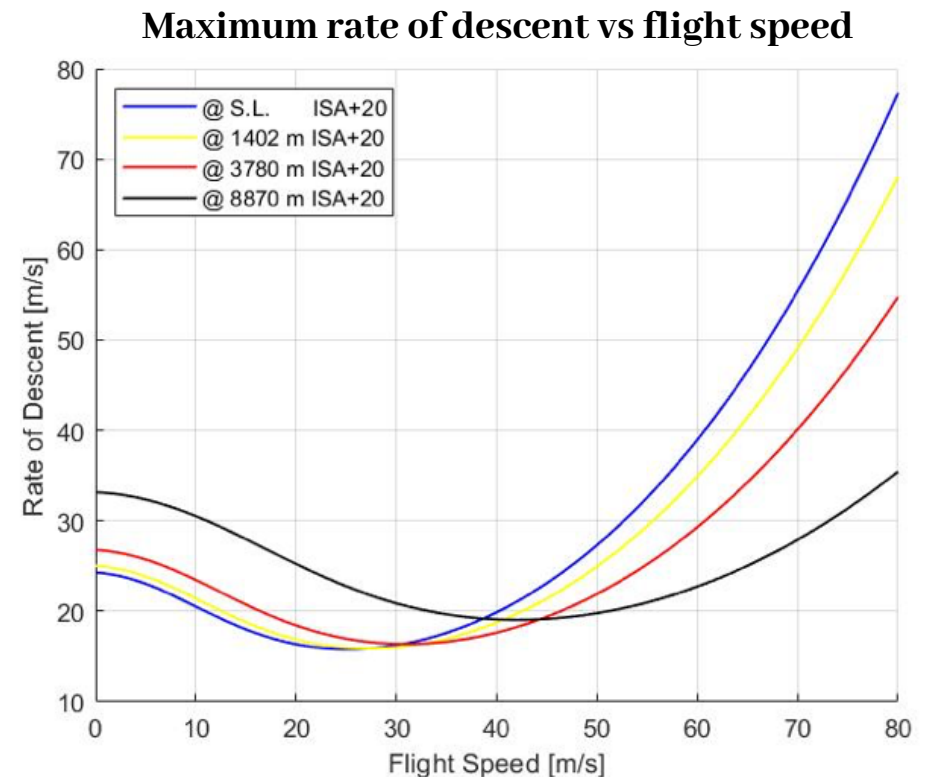
## Rate of Climb

Due to the electrical engines, the rate of climb increases significantly and the helicopter becomes extremely responsive



## Rate of Descent

Maximum rate of descent occurs when no power is being supplied to the rotors, transitioning the helicopter into autorotation.



# Performance

## Range, Endurance, and Hover Ceiling

► The battery power of the helicopter provides 32.4% of the total range and 27% of the total endurance. If the battery weight was replaced with fuel, range and endurance would increase to 366.32 km and 3.17 hours respectively. Even though there is reduction in performance from using a hybrid propulsion package, this is necessary for meeting the strict hover requirements.

### Flight characteristics for maximum range and endurance

	Range km	Endurance hours
Optimum Cruise speed	25 m/s	38 m/s
Average power at optimum cruise speed	407 kW	491 kW

## Autorotation

► Due to the large blade inertia and low disk loading, the helicopter is within the acceptable autorotation range for all key altitudes.

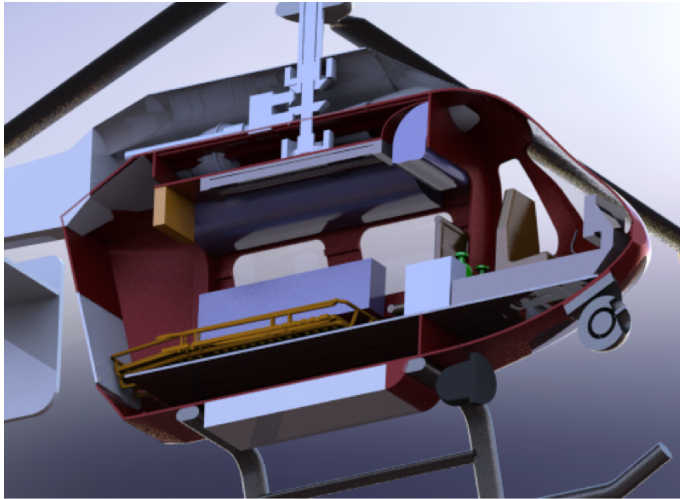
### Autorotation index vs Altitude

Altitude	Autorotative Index
Sea level	108.86
1,402 m (4,600 ft)	94.74
3,780 m (12,400 ft)	74.05
8,870 m (29,100 ft)	41.42

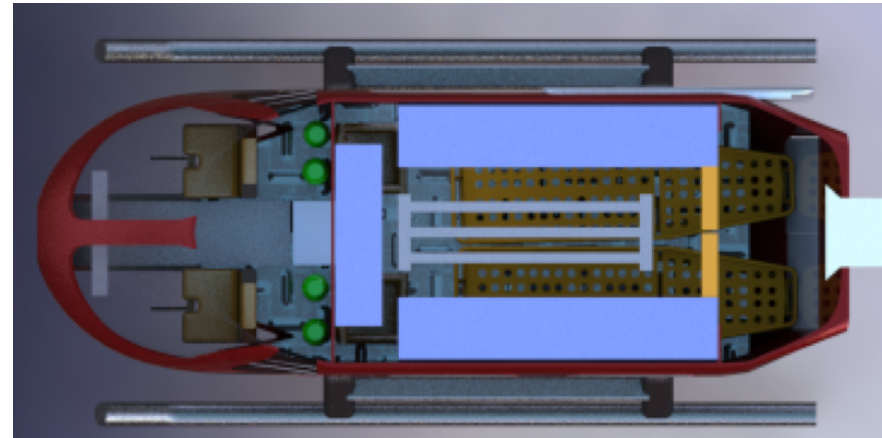


# Structure and Cabin Architecture

Fuselage Section view



Internal cabin layout



Exposed fuselage view



▮ The fuselage was initially to be made boron-epoxy, however, evaluation of the helicopter's function shows the limitations it has stepping into other search and rescue environments.

▮ This fuselage uses a mixture of glass fibre and carbon fibre composites, which still meets the weight boundaries of a boron-epoxy fuselage.

# Weight Refinement

## Component weights

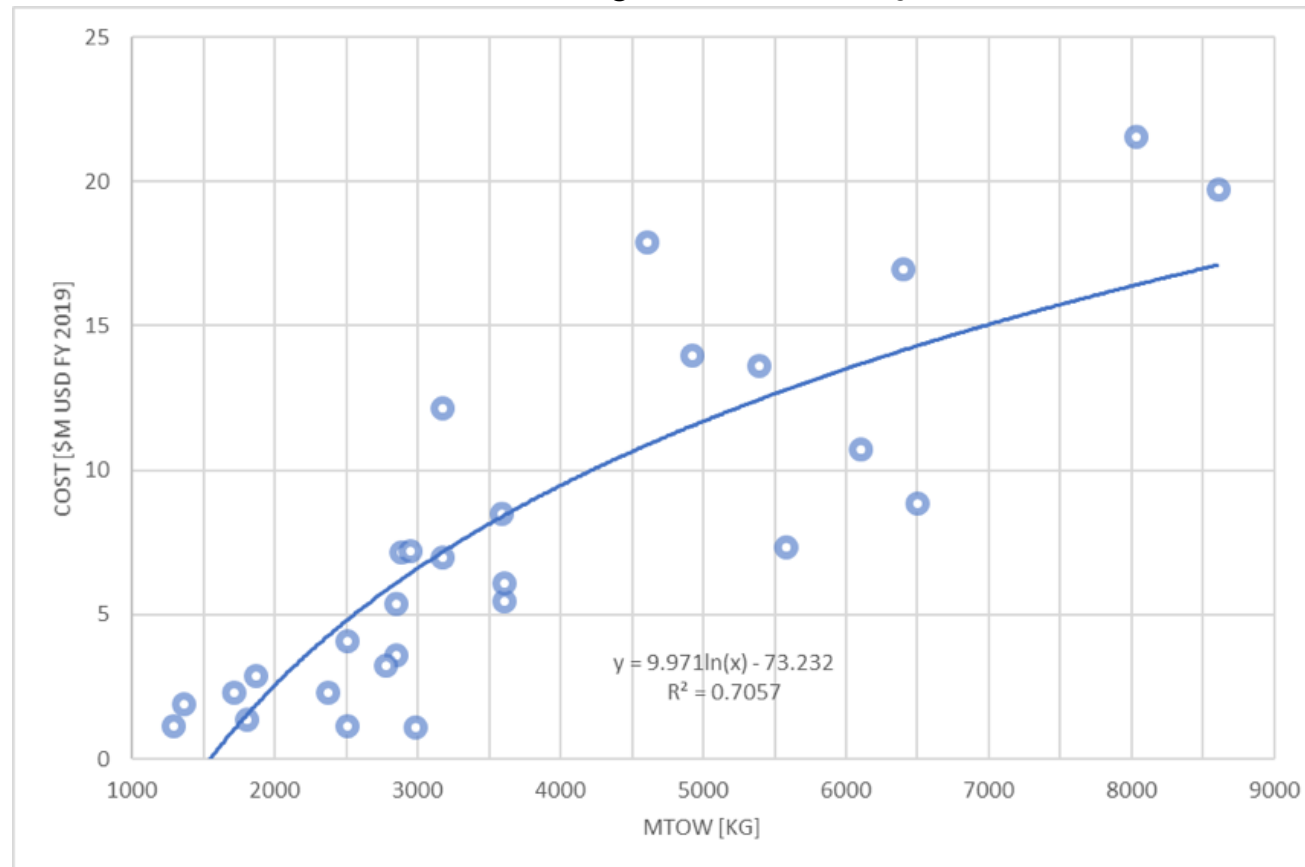
System	Mass [kg]	Mass [lbs]
Main Rotor		
<b>Rotor Blades</b>	106.27	234.27
<b>Rotor Hub</b>	72.99	160.92
Structures		
<b>Fuselage</b>	183.58	404.72
<b>Nacelles</b>	37.78	83.29
<b>Horizontal Stabiliser</b>	25.43	56.06
<b>Vertical Stabiliser</b>	17.90	39.46
<b>Landing gear</b>	128.03	282.26
<b>Furnishing</b>	61.14	134.79
<b>Manufacturing Variation</b>	10.97	24.18
Power Production and Supply		
<b>Turboshaft Engines</b>	268	590.84
<b>Fuel Weight</b>	210	462.97
<b>Electrical Engines</b>	100	220.46
<b>Batteries</b>	150	330.69
<b>Drivetrain</b>	260.44	574.17
Flight Control Systems		
<b>Avionics</b>	68.04	150
<b>Instruments</b>	16.46	36.29
<b>Systems Controls (Boosted)</b>	1.35	2.98
<b>Cockpit Systems</b>	10.69	23.62
<b>Electrical systems</b>	201.06	443.25
<b>Hydraulic Systems</b>	17.40	38.36
<b>Fuel Systems</b>	5.09	11.22
<b>Propulsion systems</b>	44.99	99.18
<b>Anti-Ice systems</b>	43.86	96.70
Mission Systems		
<b>Hoist (Goodrich 44316)</b>	50	110.23
<b>FLIR Camera (Safran Ultraforce 350-HD)</b>	28	61.73
<b>Crew Oxygen (4x MH Oxygen CFFC-048)</b>	16	35.27
<b>Searchlight (Spectrolab SX-16 Nightsun Enhanced)</b>	31	68.34
Payload Weight		
<b>Crew 1</b>	85	187.39
<b>Crew 2</b>	85	187.39
<b>Crew 3</b>	85	187.39
<b>Patient 1</b>	85	187.39
<b>Patient 2</b>	85	187.39
<b>Emergency medical Supplies</b>	150	330.69
<b>MTOW</b>	2741.48	6043.93



# Cost Breakdown

The development and unit costs are calculated using regression analysis. For unit costs, a Cost Estimating Relationship (CER) equation based on MTOW was developed. All data sourced for this regression model is sourced from Jane's, with selected helicopters listed in Appendix A. All costs are converted to \$USD FY2019 using NASA's projected inflation factors. For our design, the unit cost is estimated at *\$5.73 Million USD* per helicopter (FY2019). Note all masses used are in kg.

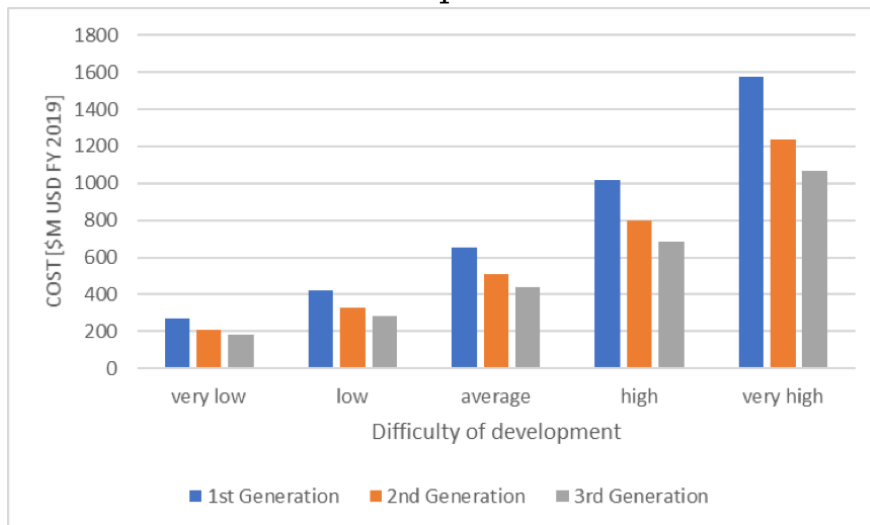
## Unit cost regression analysis



# Cost Breakdown

Development costs were estimated using the Johnson Space Centre Advanced Mission Cost Model (AMCM). This is another regression model developed by NASA, which estimates development costs based on MTOW, quantity of units produced, generation of design, and other parameters

Development costs vs difficulty of production and hardware development



Cost Breakdown vs manufacturer experience

Cost	Airbus (2 <sup>nd</sup> Gen. model)	Experienced Manufacturer	New Manufacturer
<b>Development</b>	\$327.57 Million	\$420.65 Million	\$1014.9 Million
<b>Unit</b>	\$5.73 Million	\$5.73 Million	\$5.73 Million

